

# **MULTIYEAR DROUGHTS REGIONAL ANALYSIS AND PREDICTION IN NORTH-WESTERN GREECE**

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# Project aim

**grade** previous study in the wider region  
(Mikou et al., 1993)

estimate geomorphic and climatic characteristics  
from 13 riverbasins of the study area

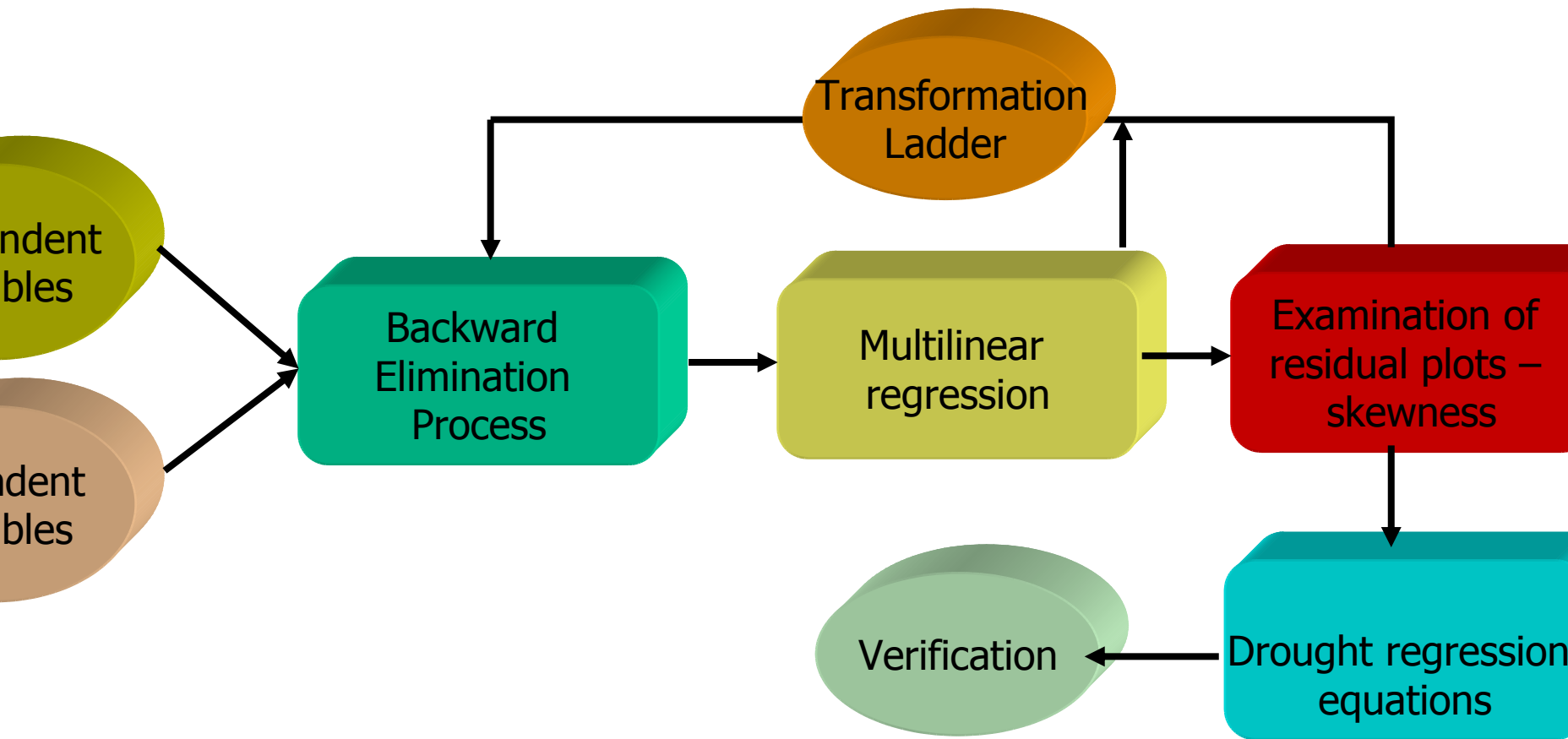
derive reliable mathematic **equations** between  
drainage characteristics and basin characteristics  
in order to apply in similar **ungauged** catchments  
in the study area

draw conclusions from the equations

# Innovations in comparison with the initial study

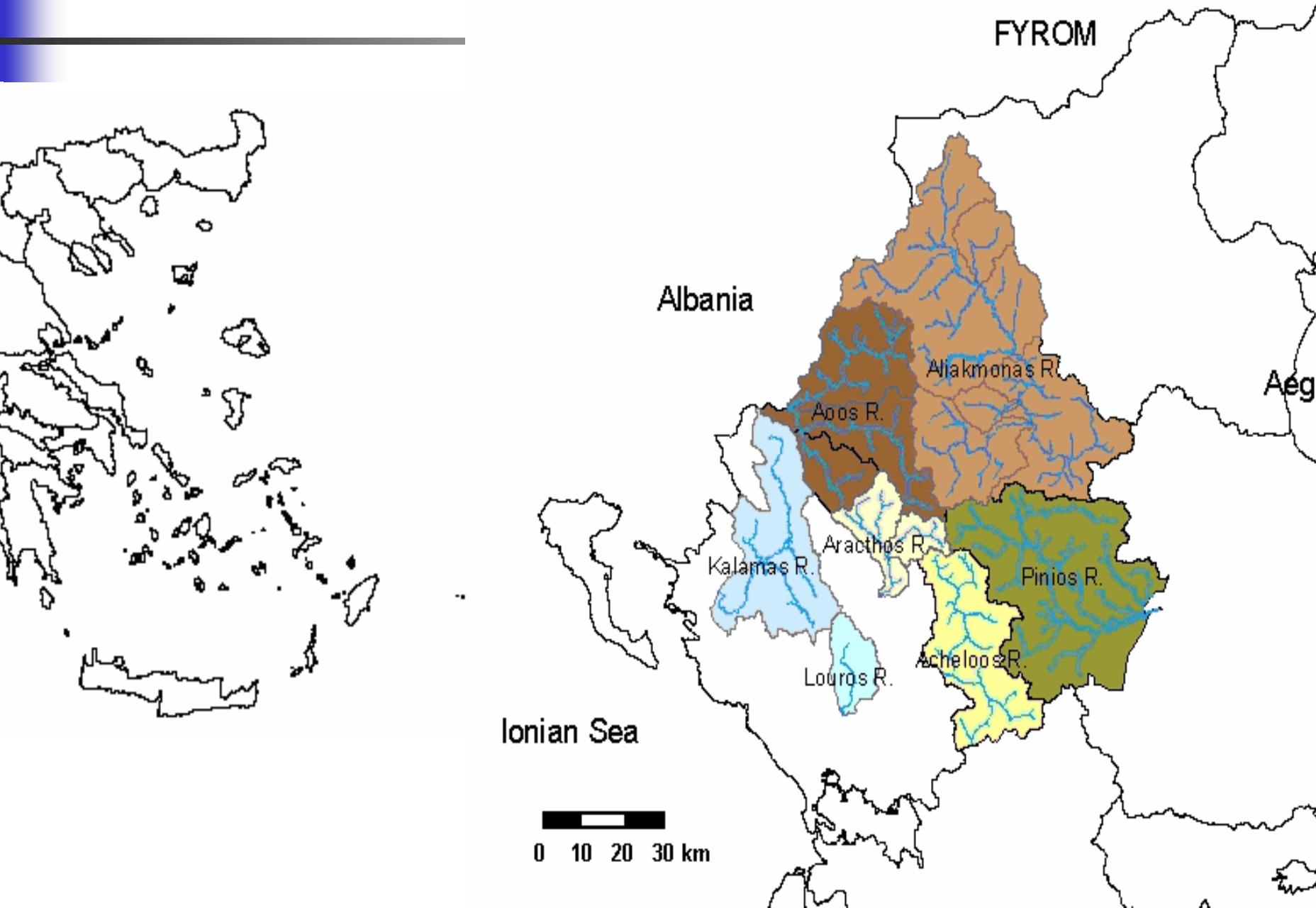
- **Verification** of regression equations in two riverbasins of the study area
- **Transformation ladder** for optimization of the final regression equations through the confrontation of skewness in the histogram of standardized residuals
- **Combined parameters** of independent variables were introduced ( $P_d$ ) – Need for restricted independent variables by the small basin sample size:  
degrees of freedom = basins - independent variables - 1
- **Alternative regression** equations derived for certain drought characteristics. Selection according to data availability

# Model



# Study Area: 14200 km<sup>2</sup>

120 hydrometeorological gauges with data P,T

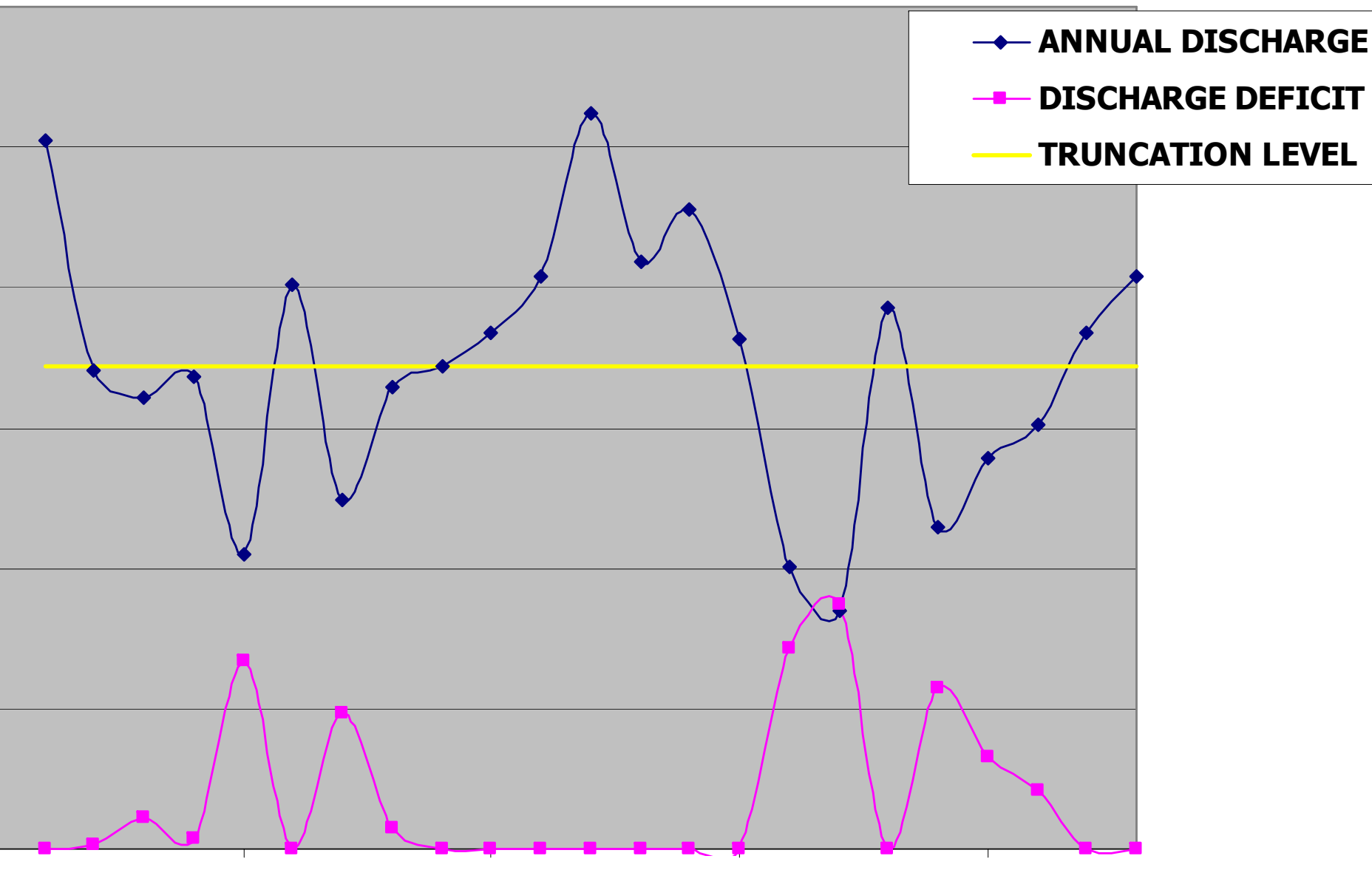


River	Drainage basin	A(km <sup>2</sup> )
Calibration		
Aliakmon	Ilarion	5005,89
Aliakmon	Siatista	2724,65
Aracthos	Plaka	970,35
Acheloos	Avlaki	1348,97
Acheloos	Sikia	1173,12
Aoos	Bourazani	2140,48
Aoos	Vovoussa	202,09
Kalamas	Kioteki	1485,67
Kalamas	Soulopoulo	661,42
Louros	Louros	345,75
Pinios	Pinios	2873,15
Verification		
Aracthos	Tsimovo	640,23

n)	Gauging stations precipitation data were acquired from the NI Thiessen polygons were constructed using the ARCGIS programme.Finally, elevation reduction was performed.P needed for the calculation of Pd and PV
n)	Dry years were defined as those with streamflow lower than truncation level for each basin.Then, the difference between mean annual areal precipitation and the mean annual a precipitation of the dry years Pd over each basin was calc
c)	Gauging stations temperature data were acquired from the NI Thiessen polygons were constructed using the ARCGIS programme.Finally, elevation reduction was performed
	It was calculated using the mean annual areal precipitation l
2)	It was calculated using the Arcgis 9 programme
m)	It was calculated using the Arcgis 9 programme
n)	It was calculated using the Arcgis 9 programme
	It was calculated using the Arcgis 9 programme

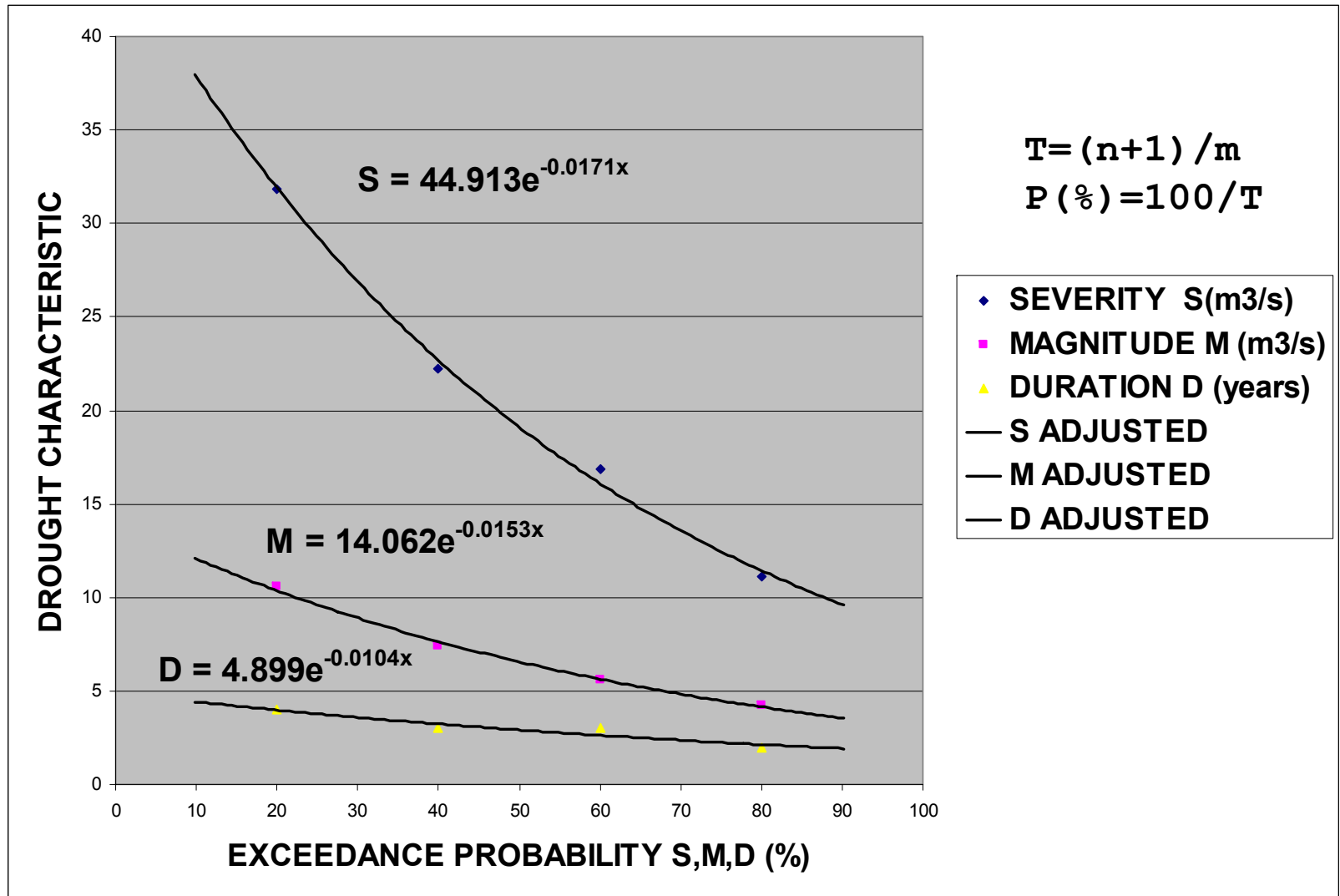
Drainage basin	P (mm)	P <sub>d</sub> (mm)	T (°C)	PV	A(km <sup>2</sup> )	PR (km)	E (m)	S	
<b>Calibration gauges</b>									
n	<b>Ilarion</b>	770,6	231,2	10,89	0,1983	5005,8	431,0	910,3	0,00234
n	<b>Siatista</b>	502,2	147,7	10,27	0,2979	2724,6	268,0	1005,3	0,00211
s	<b>Plaka</b>	1581,3	184,4	15,10	0,1011	970,3	181,8	1059,2	0,00825
s	<b>Avlaki</b>	1955,5	252,2	10,45	0,1384	1348,9	209,9	1206,2	0,00882
s	<b>Sikia</b>	2023,3	156,4	10,24	0,1312	1173,1	184,3	1172,8	0,00976
	<b>Bourazani</b>	1139,6	193,7	11,73	0,1773	2140,4	361,4	1222,7	0,02720
	<b>Vovoussa</b>	1449,0	86,4	9,98	0,1684	202,0	72,0	149,0	0,01608
s	<b>Kioteki</b>	1245,8	227,2	11,84	0,1955	1485,6	218,1	548,3	0,00581
s	<b>Soulopoulo</b>	1421,2	123,4	11,19	0,1857	661,4	116,2	649,8	0,00974
	<b>Louros</b>	1565,8	119,4	12,93	0,1784	345,7	96,0	691,4	0,04214
	<b>Pinios</b>	931,9	191,0	14,42	0,2096	2873,1	336,9	537,2	0,01976
<b>Verification gauges</b>									
s	<b>Tsimovo</b>	1693,3	208,3	10,18	0,1237	640,2	133,9	1069,7	0,00858

# ANNUAL DISCHARGE-TRUNCATION LEVEL (SYKIA)



Flood year	Discharge (m <sup>3</sup> /s)	Deficit (m <sup>3</sup> /s)	Event's Serial Number	Severity S (m <sup>3</sup> /s)	Magnitude M (m <sup>3</sup> /s)	Duration (y)
86-87	45.58	0.00				
87-88	36.33	1.93				
88-89	18.12	12.41	3	31.80	10.60	3
89-90	16.94	17.46				
90-91	38.63	0.00				
91-92	22.87	11.53				
92-93	27.90	6.50	4	22.24	7.41	3
93-94	30.19	4.21				
94-95	36.70	0.00				
95-96	40.85	0.00				

# Light characteristics - Exceedance probabilities cu



## Frequency analysis - Sort in a descending order (Sikia)

	<b>Severity S (m<sup>3</sup>/s)</b>	<b>Magnitude M (m<sup>3</sup>/s)</b>	<b>Duration D (years)</b>	<b>T</b>	<b>P%</b>
	<b>31.80</b>	<b>10.60</b>	<b>4</b>	<b>5</b>	<b>20</b>
	<b>22.24</b>	<b>7.41</b>	<b>3</b>	<b>2.5</b>	<b>40</b>

S10 (m3/s)	S50 (m3/s)	S90 (m3/s)	M10 (m3/s)	M50 (m3/s)	M90 (m3/s)	D10 years	D50 years	D90 years	MDS (m3/s)	MDM (m3/s)	MDD years	TP1	TP2
94.38	23.52	2.90	18.31	12.44	2.46	5.15	1.89	1.18	14.17	4.95	2.20	0.40	0.40
60.74	9.05	2.35	13.83	4.16	2.04	4.39	2.17	1.16	14.45	6.31	2.00	0.40	0.40
57.00	10.01	1.76	13.28	5.75	2.32	4.29	1.74	0.76	15.89	7.02	2.00	0.40	0.40
59.10	18.42	5.74	13.59	6.32	2.99	4.35	2.91	1.92	30.29	3.33	3.00	0.01	0.40
33.34	10.12	3.07	9.43	3.48	1.60	3.54	2.91	1.92	20.51	6.95	3.00	0.01	0.40
120.4	25.30	3.04	21.39	10.66	3.39	5.63	2.37	0.90	35.65	11.27	2.75	0.25	0.40
12.46	2.41	0.47	5.03	1.46	0.56	2.48	1.65	0.82	3.55	1.76	1.80	0.40	0.40
65.78	11.28	1.93	14.55	6.85	2.34	4.52	1.65	0.82	17.31	8.67	1.80	0.40	0.40
21.94	9.07	1.56	4.97	3.80	2.91	4.42	2.91	1.92	11.89	4.03	3.00	0.01	0.40
19.00	3.94	0.82	3.57	2.12	1.26	5.33	1.86	0.65	5.60	2.35	2.25	0.50	0.40
87.04	22.17	2.52	35.21	10.95	3.41	2.47	1.35	0.74	24.37	14.46	1.50	0.67	0.40

**Verification Basins**

22.50	8.24	2.00	9.23	3.27	1.43	3.50	2.50	1.46	14.70	2.70	2.75	0.01	0.40
-------	------	------	------	------	------	------	------	------	-------	------	------	------	------

t	1	2	3	4	5	6
	-7,713	-7,619	-7,200	-6,711	-5,559	-4,862
	0,89	0,95	0,71	0,50	0,48	0,52
	2,10	2,88	2,73	2,24	2,00	2,14
	0,171	0,064	0,053	0,075	0,093	<b>0,069</b>
	0,79	0,77	0,76	0,63	0,42	
	1,96	2,27	2,17	1,75	1,19	
	0,189	0,108	0,096	0,141	<b>0,208</b>	
	0,34	0,29	0,28			
	1,25	1,43	1,34			
	0,339	0,249	<b>0,253</b>			
	-0,91	-0,82	-0,93	-0,73	-0,41	-0,49
	-1,96	-2,42	-2,77	-2,26	-1,70	-2,09
	0,189	0,094	0,050	0,074	0,139	<b>0,075</b>
	2,16	2,04	2,28	2,11	1,67	1,80
	3,12	3,93	4,70	4,19	3,99	4,33
	0,089	0,029	0,009	0,009	0,007	<b>0,003</b>
	0,05					
	0,39					
	<b>0,734</b>					
	0,27	0,36				
	0,61	1,13				
	0,601	<b>0,341</b>				
	-0,387	-0,457	-0,136	-0,110		
	-0,99	-1,55	-1,76	-1,37		
	0,427	0,218	0,153	<b>0,228</b>		

$$-4,86 - 0,492 A + 1,80 PR + 0,522 Pd$$

Factor	Coef	SE Coef	T	P
Constant	-4,8624	0,8482	-5,73	0,001
A	-0,4923	0,2356	-2,09	0,075
PR	1,8049	0,4164	4,33	0,003
Pd	0,5220	0,2434	2,14	0,069

149218 R-Sq = 97,1% **R-Sq(adj) = 95,8%**

### Analysis of Variance

	DF	SS	MS	F	P
Regression	3	5,1439	1,7146	77,01	0,001
Residual Error	7	0,1559	0,0223		
Total	10	5,2997			

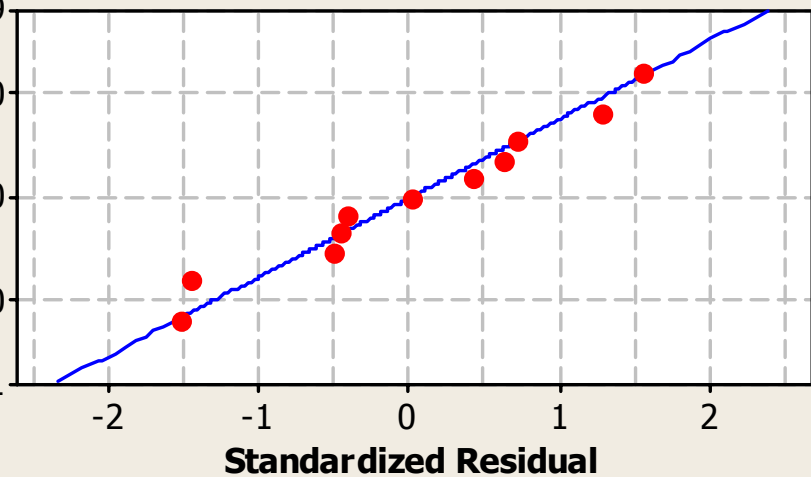
DF	Seq SS
1	4,4166
1	0,6249
1	0,1024

In the case of the regional regression analysis, the primary condition to applicability is that the basin, geomorphic and climatic characteristics should be within the range of those used to develop the regression equations. It is not wise to extrapolate the use of the regression equations to basins with characteristics outside the range of the data used to develop the equations.

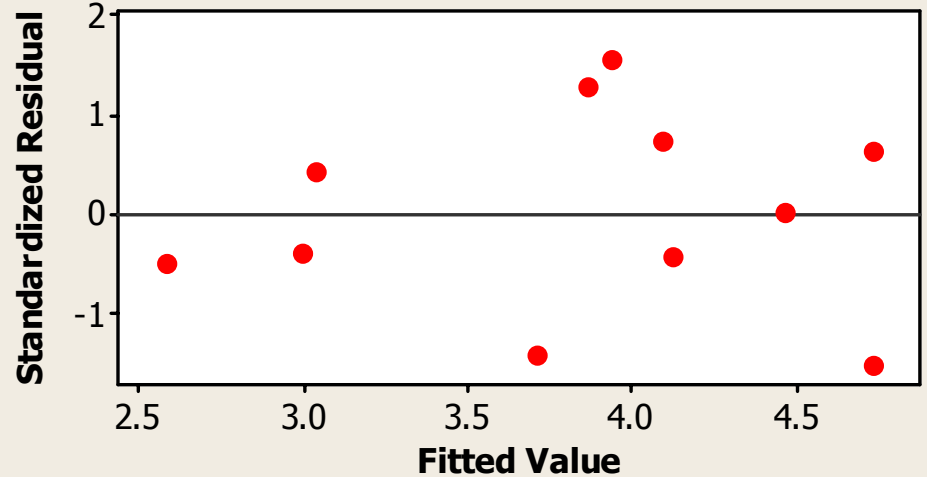
# Residual Plots

## Residual Plots for S10

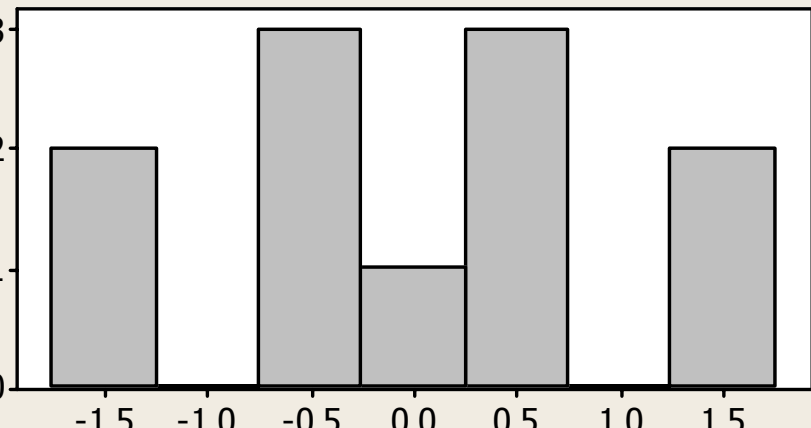
### Normal Probability Plot



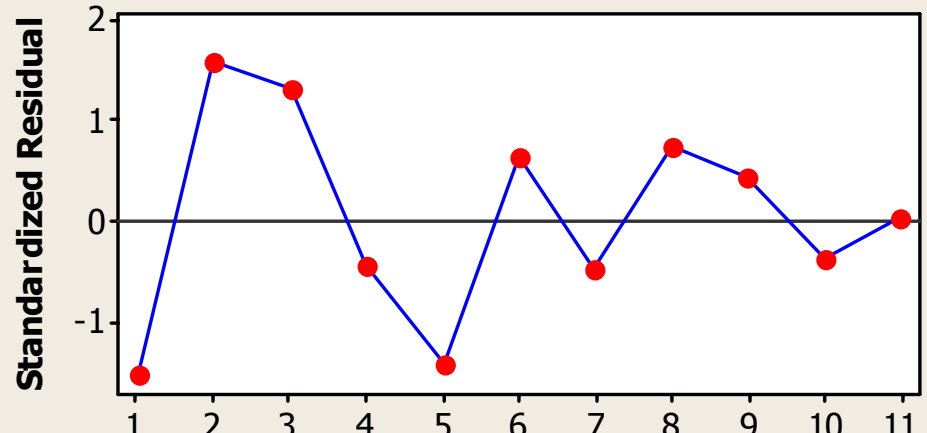
### Versus Fits



### Histogram



### Versus Order



$\theta$	Transformation	Name	Comment
	•		higher powers can be
	•		
	•		
3	$x^3$	cube	
2	$x^2$	square	
1	$x$	original units	no transformation
1/2	$\sqrt{x}$	square root	commonly used
1/3	$\sqrt[3]{x}$	cube root	commonly used
0	$\log(x)$	logarithm	commonly used. Ho place of $x^0$
-1/2	$-1/\sqrt{x}$	reciprocal root	the minus sign pres order of observati
-1	$-1/x$	reciprocal	
-2	$-1/x^2$		

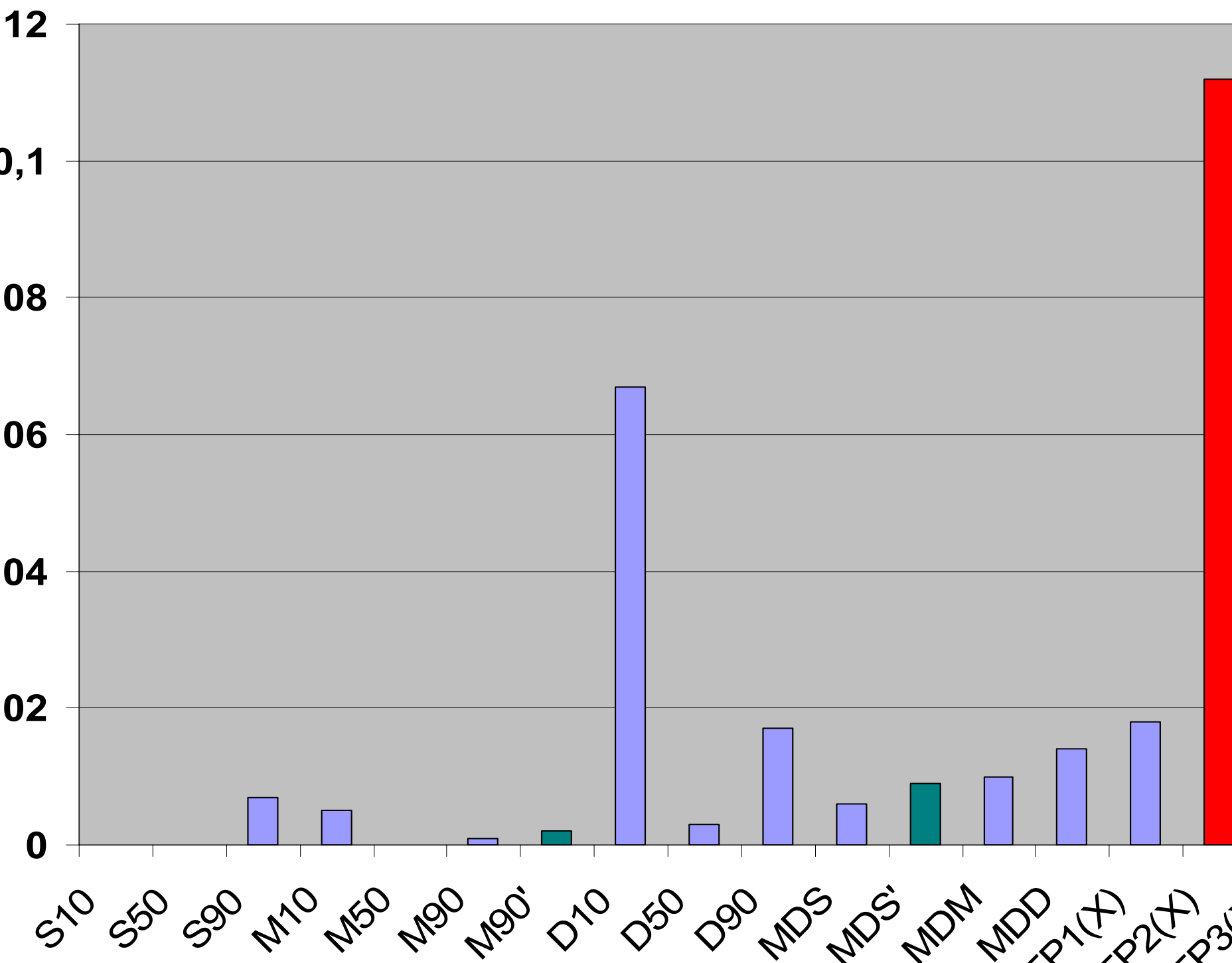
# Transformation-the ladder of power

- **Transformation ladder** for optimization of the fit equations through the confrontation of skewness in histogram of standardized residuals concerning. In specific study several transformations were examined from square and cube to reciprocal square ( $-1/x^2$ )

- $\ln Y = a_1 \ln X_1 + a_2 \ln X_2 + \dots + a_n \ln X_n$

- $TP = a_1 X_1 + a_2 X_2 + \dots + a_n X_n$



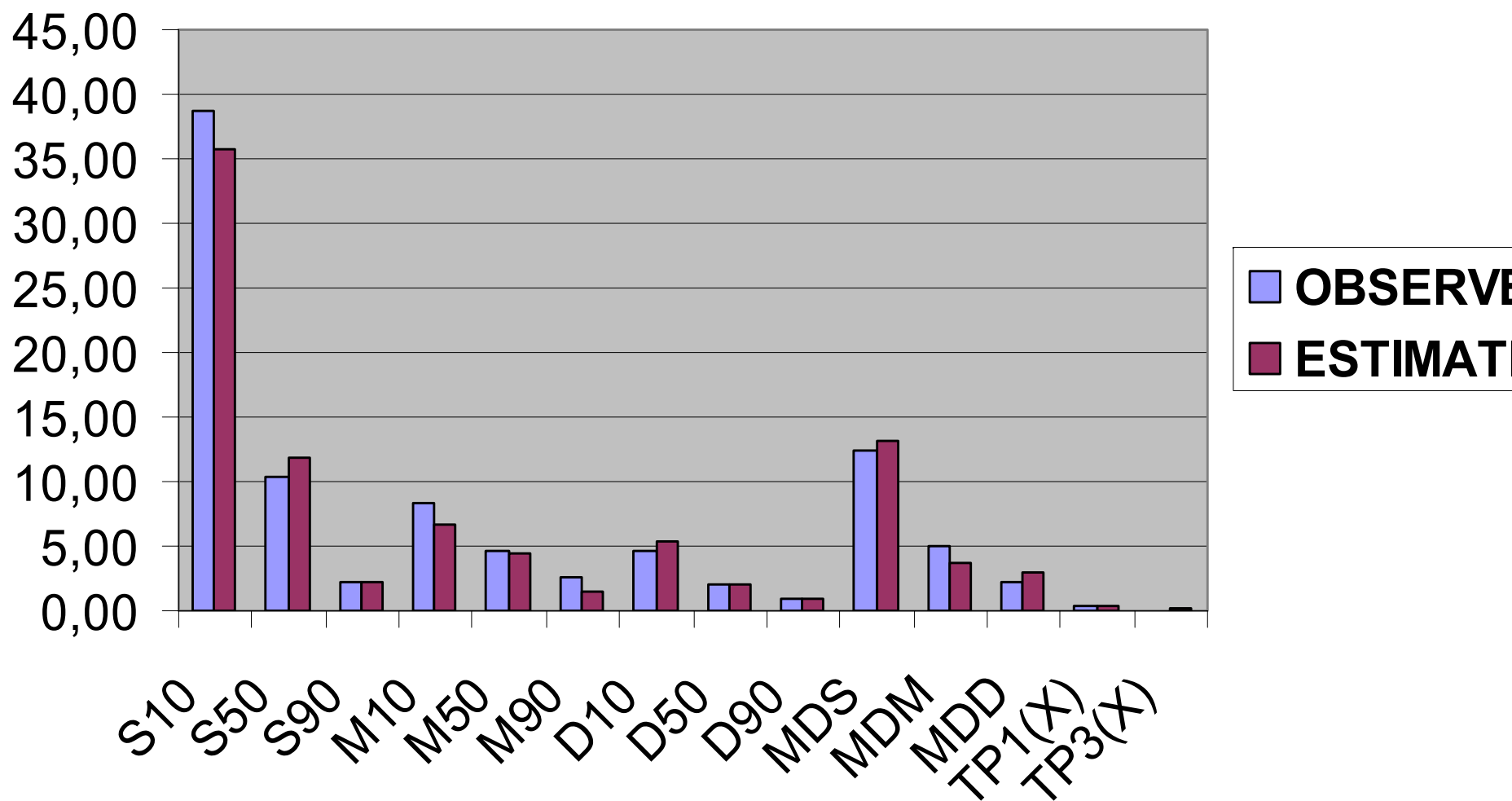


# VERIFICATION RESULTS

## MEAN PREDICTION ERROR

$$\varepsilon (\%) = [ (Y_i - \tilde{Y}_i) / Y_i ] = 16,54 \%$$

### MESOCHORA BASIN

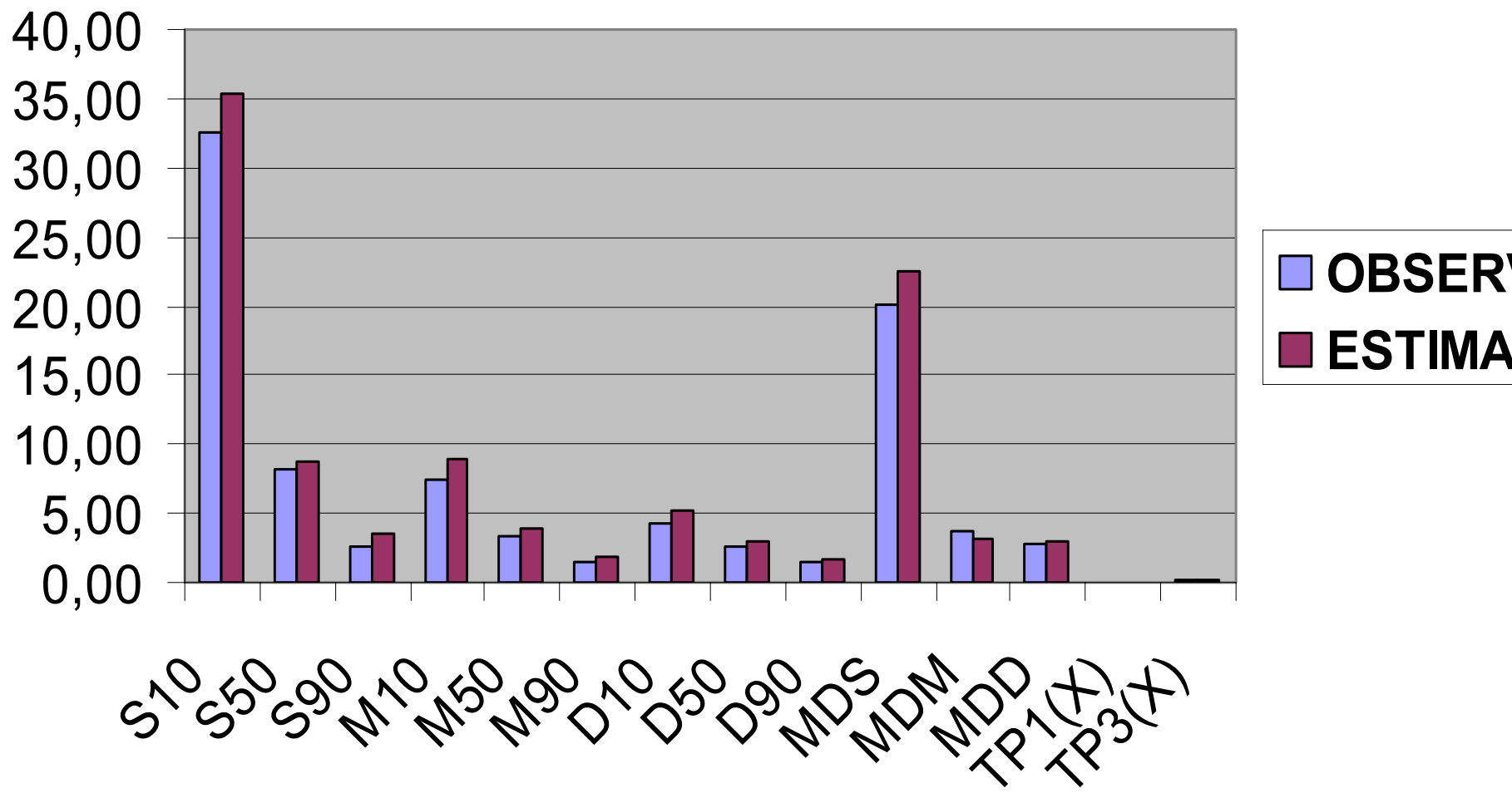


# VERIFICATION RESULTS

## MEAN PREDICTION ERROR

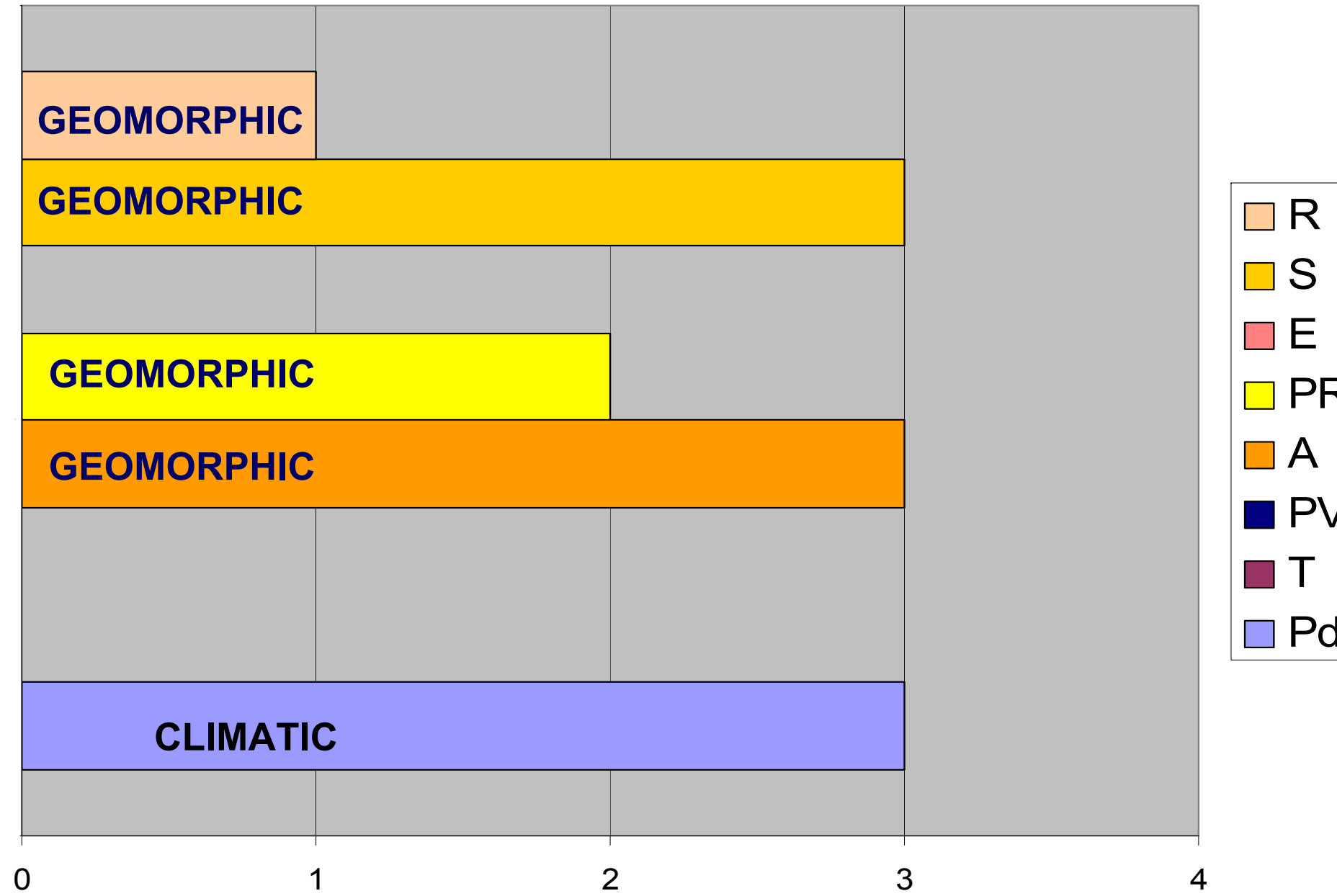
$$\varepsilon (\%) = [ (Y_i - \tilde{Y}_i) / Y_i ] = 21,55 \%$$

### TSIMOVO BASIN

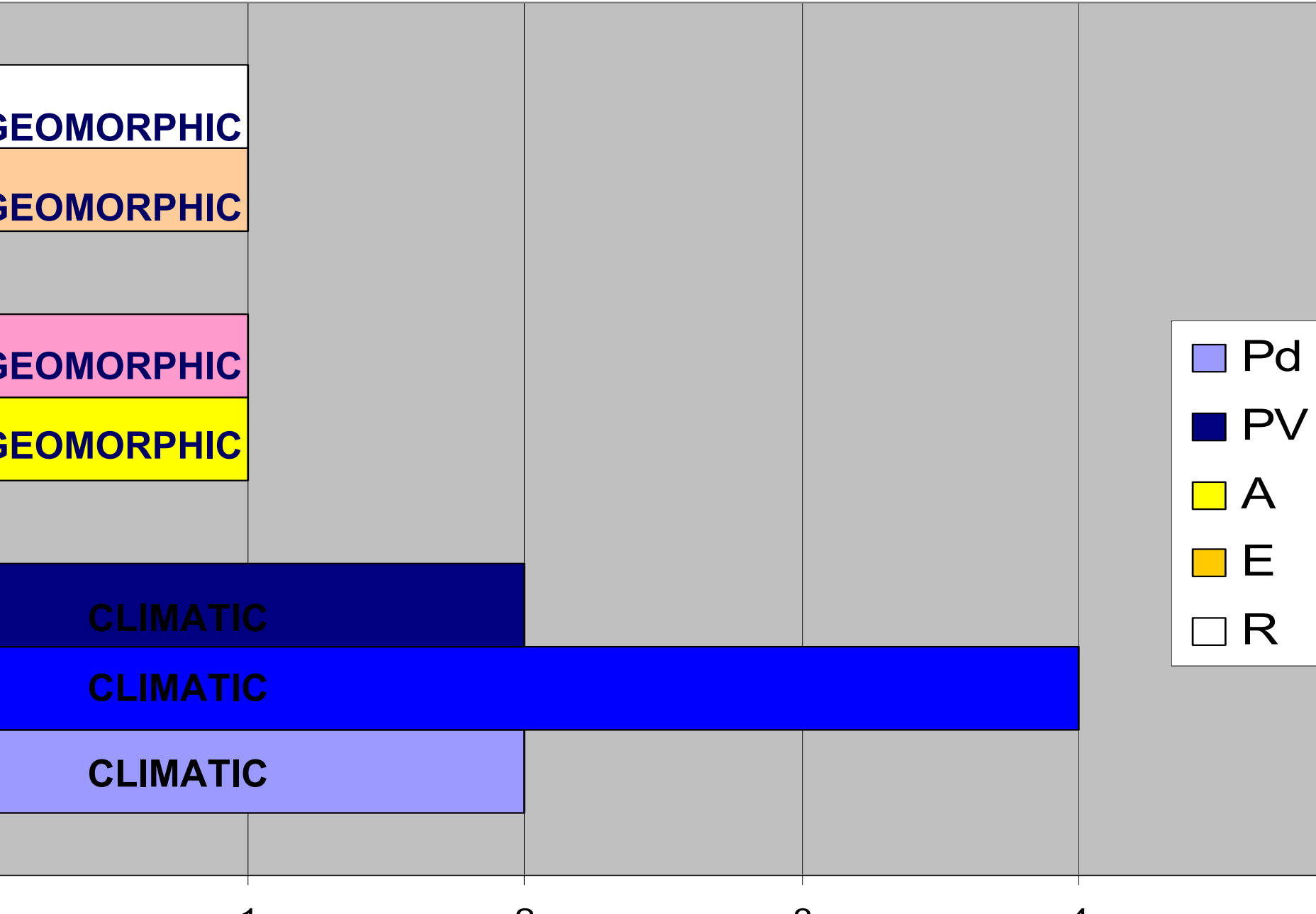


<b>Thought Characteristics</b>	<b>Significant Variable</b>	<b>P<sub>d</sub></b>	<b>T</b>	<b>P<sub>v</sub></b>	<b>A</b>	<b>PR</b>	<b>E</b>	<b>S</b>
<b>Verity S</b>	<b>1<math>\eta</math></b>	<b>2</b>			<b>1</b>	<b>2</b>		
	<b>2<math>\eta</math></b>	<b>1</b>			<b>1</b>			<b>2</b>
	<b>3<math>\eta</math></b>				<b>1</b>			<b>1</b>
	<b>Sum</b>	<b>3</b>	<b>0</b>	<b>0</b>	<b>3</b>	<b>2</b>	<b>0</b>	<b>3</b>
<b>Attitude M</b>	<b>1<math>\eta</math></b>				<b>3</b>	<b>1</b>		
	<b>2<math>\eta</math></b>	<b>1</b>		<b>1</b>		<b>1</b>	<b>1</b>	
	<b>3<math>\eta</math></b>	<b>1</b>	<b>1</b>					<b>1</b>
	<b>Sum</b>	<b>2</b>	<b>1</b>	<b>1</b>	<b>3</b>	<b>2</b>	<b>1</b>	<b>1</b>
<b>Attention D</b>	<b>1<math>\eta</math></b>	<b>2</b>	<b>2</b>	<b>1</b>			<b>0</b>	
	<b>2<math>\eta</math></b>		<b>2</b>	<b>2</b>				
	<b>3<math>\eta</math></b>				<b>1</b>	<b>1</b>		<b>1</b>
	<b>Sum</b>	<b>2</b>	<b>4</b>	<b>2</b>	<b>1</b>	<b>1</b>	<b>0</b>	<b>1</b>
<b>Attentionability TP</b>	<b>1<math>\eta</math></b>		<b>1</b>		<b>1</b>			
	<b>2<math>\eta</math></b>			<b>1</b>		<b>1</b>		

# Most significant variables – Drought severity S equations



# Most significant variables – Drought duration D equations



# Conclusions 1

- The verification results in two waterbasins of the study region proved that the constructed models function satisfactorily with precipitation or  $P_v$ , they are steadily significant in all the drought expressions - agreement with similar studies conducted in California (Pantelis et al., 1985) and Greece (Mimikou et al., 1993).
- Of the drought indices examined, **S** and **M** are determined mainly by **geomorphic** indices. On the other hand, **D** and **T** appear most closely related to **climatic factors**, although **T** seems wider than **D** in its expressions, in terms of independent variables -agreement with Mimikou, Paulson.
- The explanatory variables the most frequently occurring in the regression equations as being first, second or third most significant in order of importance are **A**, **P<sub>d</sub>** and **T**.

# Conclusions 2

- **M<sub>90</sub> & MDS: Alternative** regression equations derived. Electricity according to data availability
- In comparison to similar studies conducted in California (Paulson et al., 1985) and Greece (Mimikou et al., 1993), more precise estimating accuracy was achieved regarding **S**, **M** and especially **MDS** while a relation for **D** proved here acceptable. Comparison made using the SE of estimate.
- In addition, **S**, **M** seem to remain quite unaffected by a temperature increase, while duration characteristics (**D**, **TP**) seem to be more sensitive. That is, the droughts would tend to have more adverse characteristics in terms of duration, due to the greenhouse effect.
- A climate change in the precipitation pattern towards more extreme phenomena (**P<sub>d</sub>** increase) is estimated to result in more adverse effects in terms of increasing sensitivity regarding **S**.

# Study prospects

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- Water consumption as an input to regional model:
  - Domestic demand
  - Agricultural demand
- Advanced regression tools:
  - Partial least squares
  - Best subsets
- Application to further sets of riverbasins for equation extraction
- Addition independent variables
  - Runoff coefficient
  - Catchment's land cover (urbanization, forests)

# References

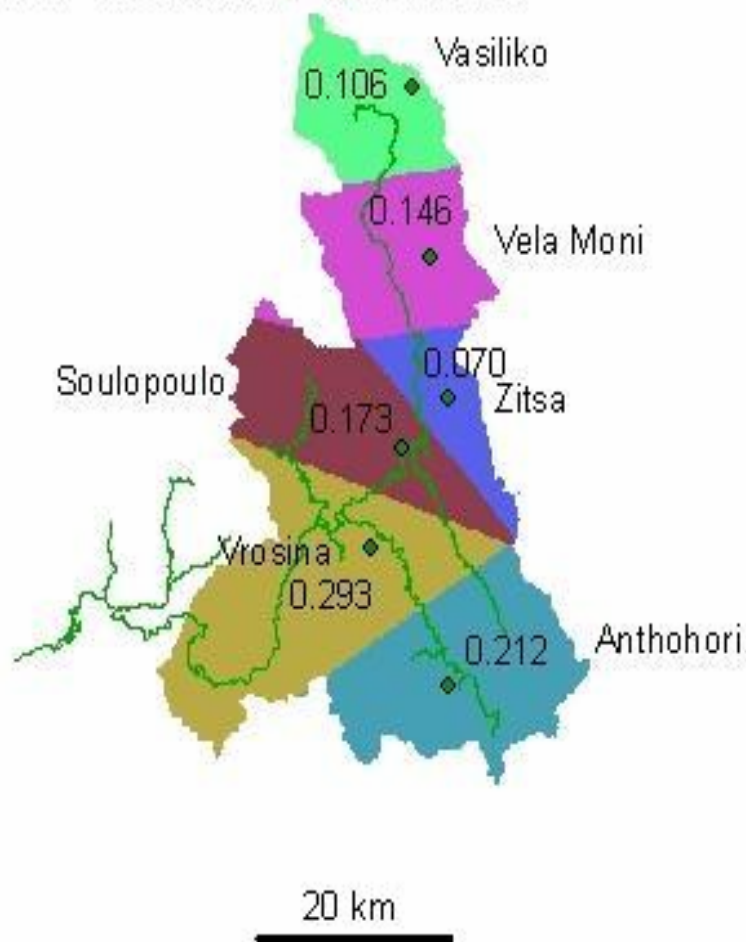
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**Thank you**

# Questions

# Thiessen Polygons- Precipitation

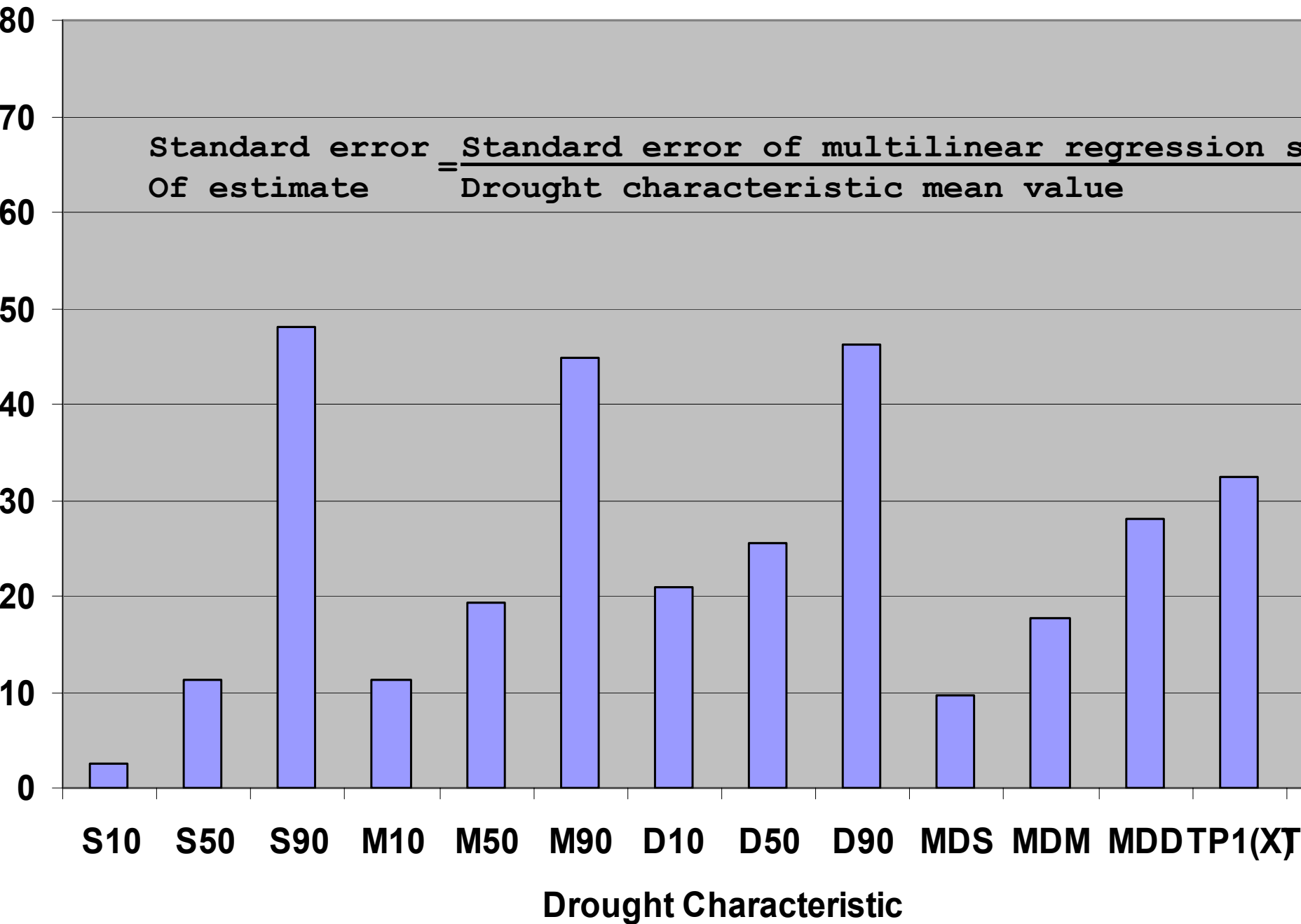
KIOTEKI THIESSEN POLYGONS - PRECIPITATION



THIESSEN POLYGONS- PRECIPITATION



# Regression's Standard Error of Estimate



# DEPENDENT VARIABLES

	<b>Pd</b>	<b>T</b>	<b>PV</b>	<b>A</b>	<b>PR</b>	<b>E</b>	<b>S</b>
	<b>0.130</b>						
	<b>-0.120</b>	<b>-0.261</b>					
	<b>0.562</b>	<b>-0.033</b>	<b>0.453</b>				
	<b>0.668</b>	<b>0.086</b>	<b>0.328</b>	<b>0.930</b>			
	<b>0.501</b>	<b>-0.740</b>	<b>-0.202</b>	<b>0.259</b>	<b>0.404</b>		
	<b>-0.371</b>	<b>0.325</b>	<b>-0.135</b>	<b>-0.385</b>	<b>-0.247</b>	<b>-0.157</b>	

Regression Analysis. P1(X) versus T, PV, E

The regression equation is

$$P1(X) = -0.953 + 1.16 T + 0.394 PV - 0.134 E \quad (m)$$

Predictor	Coef	SE Coef	T	P
Constant	-0.9534	0.8188	-1.16	0.282
T	1.1575	0.3110	3.72	0.007
PV	0.3943	0.1571	2.51	0.040
E	-0.13382	0.06969	-1.92	0.096

S = 0.132639      R-Sq = 74.2%      R-Sq(adj) = 63.1%

### Analysis of Variance

Source	DF	SS	MS	F	P
Regression	3	0.35367	0.11789	6.70	0.018
Residual Error	7	0.12315	0.01759		
Total	10	0.47682			

Source	DF	Seq SS
T	1	0.15008
PV	1	0.13872
E (m)	1	0.06486

regression equation is

$$\ln(LN) = -14.6 + 7.49 T + 3.24 PV$$

Predictor	Coef	SE Coef	T	P
Constant	-14.602	7.997	-1.83	0.105
	7.486	3.375	2.22	0.057
	3.236	1.693	1.91	0.092

S = 1.44406      R-Sq = 45.7%      R-Sq(adj) = 32.1%

### Analysis of Variance

Source	DF	SS	MS	F	P
Regression	2	14.061	7.030	3.37	0.08
Residual Error	8	16.682	2.085		
Total	10	30.743			

Source	DF	Seq SS
	1	6.444
	1	7.617

t	1	2	3	4	5	6	7
	-2,896	-2,899	-3,660	-2,972	-2,384	-2,996	-3,291
	0,64	0,63	0,66	0,32			
	0,95	1,26	1,43	0,92			
	0,442	0,297	0,227	0,398			
	-0,31	-0,30					
	-0,48	-0,59					
	0,680	0,596					
	-0,49	-0,49	-0,44	-0,46	-0,61	-0,53	-0,60
	-1,13	-1,57	-1,60	-1,65	-2,73	-2,58	-2,37
	0,376	0,214	0,184	0,159	0,034	<b>0,036</b>	<b>0,046</b>
	1,000	0,997	0,931	0,866	0,931	0,506	0,425
	1,35	1,93	2,02	1,86	2,05	7,26	5,67
	0,309	0,149	0,113	0,122	0,086	<b>0,000</b>	<b>0,000</b>
	-1,00	-1,00	-0,94	-0,72	-0,65		
	-0,91	-1,26	-1,31	-1,02	-0,95		
	0,458	0,296	0,262	0,354	0,380		
	-0,00						
	-0,01						
	0,995						
	0,699	0,696	0,702	0,231	0,231	0,162	
	1,00	1,43	1,58	2,26	2,29	2,32	
	0,421	0,247	0,189	0,073	0,062	<b>0,054</b>	
	-0,41	-0,41	-0,44				
	-0,66	-0,90	-1,09				
	0,578	0,433	0,337				
	0,227	0,186	0,170	0,173	0,171	0,170	0,211

Altitude (m) Temperature ( $^{\circ}\text{C}$ ) Mean annual rainfall(mm)Area (ha) Perimeter (Periarea (km)  
Estimated as the ratio of the watershed area to the perimeter  
Aspect (degrees) It was computed using the azimuth  
Stream slope (%) Computed as the ratio between the elevation at the point where main stream i  
first order and its length  
Watershed slope (%) Computed as the fraction of slope and the length of watershed  
Watershed length (km) Measured considering a plane parallel to the main stream  
Form factor The ratio between measured area and watershed length  
Lenwid This new variable was defined as the ratio between  
watershed length and watershed width described above  
Length of stream (km) Relief ratio Land use (ordinal)  
Soil texture (ordinal) Soil textures were classified according to U.S. Department  
of Agricultural textural classification triangle  
Soil permeability(ordinal) The soil permeability of all watersheds was  
classified in eleven categories  
UNESCO Index of aridity  
It is computed as the ratio of annual precipitation and potential evapotranspiration  
Horton form factor (dimensionless)  
It is the dimensionless ratio of watershed area A to the  
square of watershed length

# Thiessen Polygons- Temperature

## THIESSEN POLYGONS - TEMPERATURE

